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JMMC

HOW TO COMPUTE UNIFORM-DISK DIAMETERS FROM LIMB-DARKENED DIAMETERS ?

Daniel BONNEAU (daniel.bonneau@oca.eu)
OCA/FIZEAU-Grasse, Tél: 04 93 40 53 83

<p>Author : Daniel Bonneau</p> <p>Institute : OCA/FIZEAU-Grasse</p>	<p>Signature :</p> <p>Date : 14/01/2010</p>
<p>Approved by : Gilles DUVERT</p> <p>Institute : LAOG</p>	<p>Signature :</p> <p>Date : 14/01/2010</p>
<p>Released by : Sylvain LAFRASSE</p> <p>Institute : LAOG</p>	<p>Signature :</p> <p>Date : 14/01/2010</p>

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	Title typo correction.		
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	Added tables containing linear darkening coefficients for bands U, B, V, L et N ; Added explanation in section 1 on diamUD that will be computed in bands B, V, R, L, N ; Added links to new appendix tables in section 4 ; Added a new paragraph in section 5 to further discuss spectral types.		
2.2	14/01/2010	D. Bonneau	Section 3, 5, 6 and appendices
	Removed K mag limit in section 3 Detailed luminosity class conversion in section 5.1 Added I band case in section 5.3 Fixed coefficient values and results in section 6.3 Fixed title (UR replaced by U) in appendix 5		

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1 Introduction

In SearchCal, the potential calibrators selected near a science target are characterized by their angular diameter. The latter is calculated with a surface brightness method, more precisely using the color-magnitude relation V - (V-K) which has the lowest dispersion (Bonneau et al., 2006, A & A, 456.789).

In the catalog of calibrators created by SearchCal the θ_{VK} diameter given for each star thus corresponds to the limb-darkened disk diameter (θ_{LD}) independent of the wavelength.

In the list of calibrators provided to the user, ESO prefers to have explicitly the uniform disk angular diameters (θ_{UD}) for each band used for observations with the VLTI instrument AMBER (J-band, H-band and K-band), θ_{UD} [J], θ_{UD} [H] and θ_{UD} [K].

Within the framework of the preparation of instrument MATISSE of the VLTI, it appears useful to also calculate the diameters θ_{UD} [L] and θ_{UD} [N].

Interferometric observations being also realized at visible wavelengths (in particular with instrument VEGA on CHARA), the uniform diameters θ_{UD} [B], θ_{UD} [V] and θ_{UD} [R] can be also calculated.

This requires implementing an automated method of conversion of θ_{LD} to $\theta_{UD}[\lambda]$ when creating the list of calibrators from the JMMC catalog provided by SearchCal.

This conversion will be done with the hypothesis of a linear limb darkening.

2 Principle

Starting with SearchCal limb-darkened estimate:

$$\theta_{LD} = \theta_{VK}$$

A correction factor $\rho_{\theta}[\lambda] = \theta_{LD} / \theta_{UD}[\lambda]$ shall be applied to obtain $\theta_{UD}[\lambda]$.

According to Hanbury Brown et al. (1974, MNRAS, 167, 475):

$$\rho_{\theta}[\lambda] = [(1 - u_{\lambda}/3)/(1 - 7u_{\lambda}/15)]^{1/2}$$

where u_{λ} is the linear darkening coefficient obtained by the adjustment of the radial intensity distribution on the stellar disk, as a function of the wavelength, using a stellar atmosphere model characterized by the effective temperature (T_{eff}), the gravity ($\log g$) and the metallicity ([Fe/H]).

The value of the UD diameter at λ will be:

$$\theta_{UD}[\lambda] = \theta_{LD} / \rho_{\theta}[\lambda]$$

The error on $\theta_{UD}[\lambda]$ induced by this method is estimated in the section 6.

3 Determining Teff and log g from Spectral Type

For bright calibrators, SearchCal give the spectral type as the temperature class [O, B, A, F, G, K, M] and the luminosity class [supergiants (I), giants (II, III) and main sequence (IV, V)].

As first approximation, values of T_{eff} and $\log g$ can be obtained as a function of the temperature class for normal stars of « Main sequence », « Giants » and « Supergiants » from the tables in Allen's Astrophysical Quantities (Ed. A. N. Cox, 1999, hereafter AQ):

- Table 15.7 for T_{eff}
- Table 15.8 for $\log g/g_{\odot}$

AQ tables can be interpolated for the intermediate values of the temperature classes.

If the luminosity class is unknown, by default one can suppose that the star is a giant (III).

The bias introduced by this assumption is estimated in the section 6.

4 Data on limb-darkening

The linear limb-darkening coefficients in the U, B and V bands have been computed by Díaz-Cordovés, Claret and Gimenez (1995, A&AS, 110, 329)

The linear limb-darkening coefficients in the R, I, J, H and K bands have been computed by Claret, Díaz-Cordovés and Gimenez (1995, A&AS, 114, 247).

The linear limb-darkening coefficients in the L and N bands have been computed by van Hamme (1993, AJ, 106, 2096).

This authors have used the ATLAS stellar atmosphere models by Kurucz (1991, Harvard Preprint 3348) for a large domain of values of temperature $T_{eff} = 3500$ to 50000 K by 250 K steps and for surface gravities g [cm s^{-2}] $\log g = 0.0$ to 5.0 with 0.50 steps and a solar chemical composition.

The values for $u[U]$, $u[B]$ and $u[V]$ are can be taken from table 1 in Claret et al. paper at CDS (reference J/A+AS/110/329/table1).

See APPENDIX 5 "Table Díaz-Cordovés" in this document

The values for $u[R]$, $u[I]$, $u[J]$, $u[H]$ and $u[K]$ are taken from table 1 in Díaz-Cordovés et al. paper at CDS (reference J/A+AS/114/247/table1).

See APPENDIX 4 "Table Claret" in this document.

The values for $u[L]$ and $u[N]$ are taken from table 2 in van Hamme paper at CDS (reference J/AJ/106/2096/table2).

See APPENDIX 6 "Van Hamme" in this document.

5 Conversion of θ_{LD} to $\theta_{UD}[\lambda]$

5.1 Use of the spectral type

From SearchCal's spectral type one gets:

- The temperature class [O, B, A, F, G, K, M] and sub class [0,1,2,3,4,5,6,7,8,9]

- The luminosity class [I, II, III, IV, V] and sub class.

The **temperature classes** are converted in a numerical scale:

- O5 to O9 → 1 to 5
- B0 to B9 → 6 to 15
- A0 to A9 → 16 to 25
- F0 to F8 → 26 to 34
- G0 to G9 → 35 to 44
- K0 to K7 → 45 to 52
- M0 to M8 → 53 to 61

The **luminosity classes** are converted in a numerical scale:

- Ia-O, Ia-O/Ia, Ia, Ia/ab, lab, lab-b, lb, lb-II → 1
- II, II/III, III, III/IV → 2
- IV, IV/V, V, V/VI, VI → 3

See also the document "an encoding system to represent stellar spectral classes in archival database and cataolgs":

<http://www.ivoa.net/Documents/latest/SpectClasses.html>

5.2 Extraction of T_{eff} and $\log g$

- The value of the effective temperature T_{eff} is interpolated from Table AQ.15.7 according to the temperature and luminosity codes defined above.
- The value of the relative gravity $\log g/g_{\odot}$ is interpolated from Table AQ.15.8 according to the temperature and luminosity codes defined above.
- Taking for the Sun, $\log g_{\odot} = 4.378 \text{ cm s}^{-2}$ (AQ, 340/14 SUN), one has the surface gravity :

$$\log g [\text{cm s}^{-2}] = \log g/g_{\odot} + 4.378$$

5.3 How to compute the diameters $\theta_{UD}[I]$, $\theta_{UD}[J]$, $\theta_{UD}[H]$ and $\theta_{UD}[K]$

- T_{eff} and $\log g$ are used to get $u[I]$, $u[J]$, $u[H]$ and $u[K]$ from ClaretTable.
- Correction factors $\rho_{\theta}[I]$, $\rho_{\theta}[J]$, $\rho_{\theta}[H]$ and $\rho_{\theta}[K]$ are obtained using Hanbury Brown et al. Formula.
- Uniform disk diameters are thus :

$$\begin{aligned} \theta_{UD}[I] &= \theta_{VK} / \rho_{\theta}[I], \quad \theta_{UD}[J] = \theta_{VK} / \rho_{\theta}[J], \\ \theta_{UD}[H] &= \theta_{VK} / \rho_{\theta}[H] \text{ and } \theta_{UD}[K] = \theta_{VK} / \rho_{\theta}[K] \end{aligned}$$

5.4 How to compute the diameters $\theta_{UD}[B]$, $\theta_{UD}[V]$ and $\theta_{UD}[R]$

- T_{eff} and $\log g$ are used to get $u[B]$, $u[V]$ and $u[R]$ from "Table Díaz-Cordovés" and "Table Claret" respectively.
- Correction factors $\rho_{\theta}[B]$, $\rho_{\theta}[V]$ and $\rho_{\theta}[R]$ are obtained using Hanbury Brown et al. Formula.
- Uniform disk diameters are thus :

$$\theta_{UD}[B] = \theta_{VK} / \rho_{\theta}[B], \quad \theta_{UD}[V] = \theta_{VK} / \rho_{\theta}[V] \text{ and } \theta_{UD}[R] = \theta_{VK} / \rho_{\theta}[R]$$

5.5 How to compute the diameters $\theta_{UD}[L]$ and $\theta_{UD}[N]$

- T_{eff} and $\log g$ are used to get $u[L]$ and $u[N]$ from the "Table van Hamme"..
- Correction factors $\rho_{\theta}[L]$ and $\rho_{\theta}[N]$ are obtained using Hanbury Brown et al. Formula.
- Uniform disk diameters are thus :

$$\theta_{UD}[L] = \theta_{VK} / \rho_{\theta}[L] \text{ and } \theta_{UD}[N] = \theta_{VK} / \rho_{\theta}[N]$$

Warning:

A star having a circumstellar dusty disc or envelope must be rejected as a bad calibrator because the computation of the photometric diameter can be biased by the circumstellar radiation.

Such an object is revealed by a photometry presenting a strong infrared excess. These objects are among evolved stars (like M type giant and super giants or B[e] stars) and among young stellar objects of any spectral type.

6 Tests and Examples

6.1 HD 199947

SpType K3III cut in:

⇒ Temperature class: K3 = 48

⇒ Luminosity class: III = 2

Diam_vk = θ_{LD} = 1.185 ± 0.082 mas

1- Temperature and gravity.

From table 2 one gets with numSp = 48:

⇒ Teff = 4250 K

⇒ Log g/g_⊙ = -2.4 i.e., log g = 1.98

2- Limb-Darkening coefficients.

In Claret's table with Teff = 4250 K and log g = 1.98 one gets:

For [| (4250 – Teff) | ≤ 125] ⇒ Teff = 4250 K

For [| (1.98 – log g) | ≤ 0.25] ⇒ log g = 2.00

For Teff = 4250 K and log g = 2.00 one gets:

the coefficients u(J) = 0.501, u(H) = 0.418 and u(K) = 0.354

3- Uniform-Disk diameters.

u(J) = 0.501 ⇒ $\rho_{\theta}[J]$ = 1.043 ⇒ $\theta_{UD}[J]$ = 1.136 mas

u(H) = 0.418 ⇒ $\rho_{\theta}[H]$ = 1.034 ⇒ $\theta_{UD}[H]$ = 1.146 mas

u(K) = 0.354 ⇒ $\rho_{\theta}[K]$ = 1.028 ⇒ $\theta_{UD}[K]$ = 1.153 mas

This star is in the Mérand's catalog (Mérand et al. 2005, A&A 433, 1155):

TypSp = K3 III

θ_{LD} = 1.215 mas

$\theta_{LD} - \theta_{VK}$ = 0.030 mas

$\theta_{UD}[J]$ = 1.161

$\Delta\theta[J]$ = 0.025 mas

$\theta_{UD}[H]$ = 1.178

$\Delta\theta[H]$ = 0.032 mas

$\theta_{UD}[K]$ = 1.183 ± 0.016

$\Delta\theta[K]$ = 0.030 mas

6.2 HD 188154

SpType K5 III cut in:

⇒ Temperature class K5 = 50

⇒ Luminosity class III = 2

Diam_vk = θ_{LD} = 2.604 ± 0.18 mas

1- Temperature and gravity.

From table 2 one gets with numSp = 50:

⇒ Teff = 4050 K

⇒ Log g/g_⊙ = -2.70 i.e. log g = 1.68

2- Limb-Drakening coefficients.

In Claret's table with Teff = 4050 K and log g = 1.68 one gets:

For [| (4050 – Teff) | ≤ 125] ⇒ Teff = 4000 K

For [| (1.68 – log g) | ≤ 0.25] ⇒ log g = 1.50

For Teff = 4000 K and log g = 1.50 one gets:

the coefficients u(J) = 0.520, u(H) = 0.441 and u(K) = 0.370

3-Uniform-Disk diameters.

u(J) = 0.520 ⇒ $\rho_{\theta}[J]$ = 1.041 ⇒ $\theta_{UD}[J]$ = 2.492 mas

u(H) = 0.441 ⇒ $\rho_{\theta}[H]$ = 1.036 ⇒ $\theta_{UD}[H]$ = 2.513 mas

u(K) = 0.370 ⇒ $\rho_{\theta}[K]$ = 1.029 ⇒ $\theta_{UD}[K]$ = 2.530 mas

This star is in the Bordé's catalog (Bordé et al. 2002, A&A 393,183):

typSp = K5 III , Teff = 4046 K, log g = 1.93

θ_{LD} = 2.52 ± 0.28 mas

$\theta_{LD} - \theta_{VK}$ = -0.084 mas

u[J] = 0.506 $\theta_{UD}[J]$ = 2.42

$\Delta\theta[J]$ = -0.072 mas

u[H] = 0.433 $\theta_{UD}[H]$ = 2.43

$\Delta\theta[J]$ = -0.083 mas

u[K] = 0.367 $\theta_{UD}[JK]$ = 2.45

$\Delta\theta[J]$ = -0.080 mas

6.3 HD178524

SpType F2II/ III cut in:

⇒ Temperature class F2 = 28

⇒ Luminosity class II ou III = 2

Diam_vk = θ_{LD} = 1.754 ± 0.121 mas

1- Temperature and gravity.

From table 2 one gets with numSp = 28:

⇒ Teff = 6500 K

⇒ Log g/g_⊙ = -1.25 i.e. log g = 3.13

2- Limb-Drakening coefficients.

In Claret's table with Teff = 6500 K and log g = 3.13 one gets:

For [| (6500 – Teff) | ≤ 125] ⇒ Teff = 6500 K

For [| (3.13 – log g) | ≤ 0.25] ⇒ log g = 3.00

For Teff = 6500 K and log g = 3.00 one gets:

the coefficients u(J) = 0.314, u(H) = 0.245 et u(K) = 0.217

3-Uniform-Disk diameters.

$$u(J) = 0.314 \Rightarrow \rho_{\theta}[J] = 1.024 \Rightarrow \theta_{UD}[J] = 1.712 \text{ mas}$$

$$u(H) = 0.245 \Rightarrow \rho_{\theta}[H] = 1.018 \Rightarrow \theta_{UD}[H] = 1.723 \text{ mas}$$

$$u(K) = 0.217 \Rightarrow \rho_{\theta}[K] = 1.016 \Rightarrow \theta_{UD}[K] = 1.726 \text{ mas}$$

Bias due to uncertainty on the luminosity class

Taking the temperature class F2 = 28

The luminosity class is supposed to be unknown

1) Assuming a **"supergiant" luminosity class I = 1**

In Table 1 we get: $T_{\text{eff}} = 7030 \text{ K}$ and $\log g/g_{\odot} = -2.9$

In Table "Claret" then we get $T_{\text{eff}} = 7000$ and $\log g = 1.5$

And we obtain:

$$u(J) = 0.328 \Rightarrow \theta_{UD}[J] = 1.710 \text{ mas}$$

$$u(H) = 0.264 \Rightarrow \theta_{UD}[H] = 1.720 \text{ mas}$$

$$u(K) = 0.223 \Rightarrow \theta_{UD}[K] = 1.726 \text{ mas}$$

2) Assuming a **"dwarf" luminosity class V = 3**

In Table 3 we get: $T_{\text{eff}} = 7000 \text{ K}$ and $\log g/g_{\odot} = -0.10$

In Table "Claret" then we get $T_{\text{eff}} = 7000$ and $\log g = 4.5$

And we obtain:

$$u(J) = 0.302 \Rightarrow \theta_{UD}[J] = 1.714 \text{ mas}$$

$$u(H) = 0.239 \Rightarrow \theta_{UD}[H] = 1.723 \text{ mas}$$

$$u(K) = 0.212 \Rightarrow \theta_{UD}[K] = 1.727 \text{ mas}$$

The comparison of these values of θ_{UD} with these obtained using the true luminosity class of this star shows a difference always $< 0.012 \text{ mas}$.

6.4 Estimate of the uncertainty on θ_{UD} given the choice of T_{eff} and $\log g$ parameters

- If the temperature class and luminosity class are known:

Various trails show that:

- Taking $\log g \pm 0.5$ the change in diameter value is $\Delta\theta \leq 0.001 \text{ mas}$
- Taking $T_{\text{eff}} \pm 250\text{K}$ the change in diameter value is $\Delta\theta \leq 0.005 \text{ mas}$

- If the luminosity class is unknown, the choice of the class III seems to be reasonable.

The uncertainty on the limb-darkened diameter dominates the whole transformations.

There is no need to interpolate Claret's table for all practical purposes.

APPENDIX 1: Tables of T_{eff} and $\log g/g_{\odot}$ for Dwarfs

The initial values of this table are those of Tables 15.7 (T_{eff}) and 15.8 ($\log g/g_{\odot}$) in Allen's AQ (1999). Additional values have been added by interpolation to fill the empty ranges in the parent table.

Table 3

Sp	numSp	Teff	log g/g _s
O5	1	42000	-0,40
O6	2	41000	-0,45
O7	3	39000	-0,50
O8	4	37000	-0,50
O9	5	34000	-0,50
B0	6	30000	-0,50
B1	7	24000	-0,50
B2	8	20900	-0,50
B3	9	19000	-0,50
B4	10	17500	-0,45
B5	11	15200	-0,40
B6	12	14000	-0,40
B7	13	12500	-0,40
B8	14	11400	-0,40
B9	15	10500	-0,35
A0	16	9790	-0,30
A1	17	9500	-0,25
A2	18	9000	-0,20
A3	19	8600	-0,20
A4	20	8400	-0,15
A5	21	8180	-0,15
A6	22	7750	-0,15
A7	23	7600	-0,15
A8	24	7500	-0,10
A9	25	7350	-0,10
F0	26	7300	-0,10
F1	27	7150	-0,10
F2	28	7000	-0,10
F3	29	6900	-0,10
F4	30	6800	-0,10
F5	31	6650	-0,10
F6	32	6500	-0,05
F7	33	6200	-0,05
F8	34	6250	-0,05
G0	35	5940	-0,05
G1	36	5900	0,00
G2	37	5790	0,00
G3	38	5700	0,00
G4	39	5650	0,00
G5	40	5560	0,05
G6	41	5500	0,05
G7	42	5300	0,05
G8	43	5310	0,05
G9	44	5250	0,05
K0	45	5150	0,05
K1	46	4800	0,10
K2	47	4830	0,10
K3	48	4700	0,10
K4	49	4550	0,10
K5	50	4410	0,10
K6	51	4200	0,15
K7	52	4000	0,15
M0	53	3840	0,15
M1	54	3700	0,20
M2	55	3520	0,25
M3	56	3400	0,30
M4	57	3300	0,40
M5	58	3170	0,50

APPENDIX 2: Table of T_{eff} and $\log g/g_{\odot}$ for Giants

The initial values of this table are those of Tables 15.7 (T_{eff}) and 15.8 ($\log g/g_{\odot}$) in Allen's AQ (1999). Additional values have been added by interpolation to fill the empty ranges in the parent table.

For T_{eff} some values have been added by extrapolation for stars hotter than G5.

Table 2

Sp	numSp	Teff	$\log g/g_{\odot}$
O5	1		
O6	2		
O7	3		
O8	4		
O9	5	32000	
B0	6	26000	-1,10
B1	7	23000	-1,00
B2	8	20000	-1,00
B3	9	17000	-1,00
B4	10	15500	-1,00
B5	11	14000	-0,95
B6	12	13000	-1,00
B7	13	12000	-1,00
B8	14	11100	-1,00
B9	15	10500	-1,00
A0	16	9980	-1,00
A1	17	9600	-1,00
A2	18	9380	-1,00
A3	19	9000	-1,00
A4	20	8750	-1,05
A5	21	8500	-1,10
A6	22	8250	-1,10
A7	23	8000	-1,10
A8	24	7600	-1,10
A9	25	7400	-1,20
F0	26	7000	-1,20
F1	27	6750	-1,20
F2	28	6500	-1,25
F3	29	6300	-1,30
F4	30	6100	-1,30
F5	31	6000	-1,35
F6	32	5900	-1,40
F7	33	5800	-1,40
F8	34	5700	-1,45
G0	35	5600	-1,50
G1	36	5500	-1,50
G2	37	5400	-1,60
G3	38	5250	-1,70
G4	39	5150	-1,80
G5	40	5050	-1,90
G6	41	4950	-2,00
G7	42	4900	-2,10
G8	43	4800	-2,15
G9	44	4700	-2,20
K0	45	4660	-2,30
K1	46	4500	-2,30
K2	47	4390	-2,35
K3	48	4250	-2,40
K4	49	4150	-2,50
K5	50	4050	-2,70
K6	51	3950	-2,80
K7	52	3850	-2,95
M0	53	3690	-3,10
M1	54	3600	-3,30
M2	55	3540	-3,55
M3	56	3500	-3,75
M4	57	3400	-4,10
M5	58	3380	-4,50

APPENDIX 3: Table of T_{eff} and $\log g/g_{\odot}$ for Super Giants

The initial values of this table are those of Tables 15.7 (T_{eff}) and 15.8 ($\log g/g_{\odot}$) in Allen's AQ (1999). Additional values have been added by interpolation to fill the empty ranges in the parent table.

Table 1

Sp	numSp	Teff	log g/gs
O5	1		-1,1
O6	2		-1,2
O7	3		-1,2
O8	4		-1,2
O9	5	32000	-1,4
B0	6	26000	-1,6
B1	7	21000	-1,7
B2	8	17600	-1,8
B3	9	15500	-1,9
B4	10	14500	-2,0
B5	11	13600	-2,0
B6	12	12500	-2,1
B7	13	11700	-2,2
B8	14	11100	-2,2
B9	15	10500	-2,3
A0	16	9980	-2,3
A1	17	9600	-2,3
A2	18	9380	-2,3
A3	19	9000	-2,4
A4	20	8750	-2,4
A5	21	8610	-2,4
A6	22	8250	-2,5
A7	23	8150	-2,6
A8	24	7900	-2,6
A9	25	7600	-2,7
F0	26	7460	-2,7
F1	27	7300	-2,8
F2	28	7030	-2,9
F3	29	6950	-2,9
F4	30	6750	-2,9
F5	31	6370	-3,0
F6	32	6250	-3,0
F7	33	6150	-3,0
F8	34	5750	-3,0
G0	35	5370	-3,1
G1	36	5250	-3,2
G2	37	5190	-3,2
G3	38	5100	-3,2
G4	39	4970	-3,3
G5	40	4930	-3,3
G6	41	4800	-3,3
G7	42	4750	-3,4
G8	43	4700	-3,4
G9	44	4600	-3,5
K0	45	4550	-3,5
K1	46	4400	-3,6
K2	47	4310	-3,7
K3	48	4250	-3,8
K4	49	4100	-4,0
K5	50	3990	-4,1
K6	51	3800	-4,2
K7	52	3700	-4,3
M0	53	3620	-4,3
M1	54	3500	-4,4
M2	55	3370	-4,5
M3	56	3250	-4,6
M4	57	3000	-4,7
M5	58	2880	-4,8

APPENDIX 5: Table of $u_\theta[U]$, $u_\theta[B]$, and $u_\theta[V]$

Table Díaz-Cordovés

No	logg cm/s ²	Teff K	u(U)	u(B)	u(V)						
1	0.00	3500	0.749	0.869	0.901	67	0.00	5000	0.860	0.839	0.742
2	0.50	3500	0.769	0.889	0.901	68	0.50	5000	0.887	0.854	0.751
3	1.00	3500	0.793	0.904	0.897	69	1.00	5000	0.908	0.866	0.757
4	1.50	3500	0.813	0.913	0.890	70	1.50	5000	0.923	0.871	0.759
5	2.00	3500	0.828	0.918	0.882	71	2.00	5000	0.931	0.873	0.761
6	2.50	3500	0.833	0.916	0.873	72	2.50	5000	0.935	0.874	0.764
7	3.00	3500	0.827	0.899	0.853	73	3.00	5000	0.933	0.872	0.766
8	3.50	3500	0.787	0.831	0.797	74	3.50	5000	0.927	0.870	0.769
9	4.00	3500	0.739	0.757	0.733	75	4.00	5000	0.914	0.865	0.771
10	4.50	3500	0.708	0.713	0.690	76	4.50	5000	0.897	0.860	0.771
11	5.00	3500	0.692	0.692	0.663	77	5.00	5000	0.875	0.852	0.770
12	0.00	3750	0.828	0.902	0.894	78	0.00	5250	0.825	0.817	0.714
13	0.50	3750	0.836	0.916	0.896	79	0.50	5250	0.848	0.831	0.721
14	1.00	3750	0.845	0.925	0.893	80	1.00	5250	0.868	0.840	0.725
15	1.50	3750	0.853	0.928	0.886	81	1.50	5250	0.884	0.846	0.729
16	2.00	3750	0.856	0.927	0.876	82	2.00	5250	0.895	0.847	0.730
17	2.50	3750	0.850	0.920	0.864	83	2.50	5250	0.903	0.848	0.733
18	3.00	3750	0.838	0.908	0.849	84	3.00	5250	0.906	0.846	0.734
19	3.50	3750	0.811	0.877	0.819	85	3.50	5250	0.907	0.845	0.737
20	4.00	3750	0.761	0.802	0.751	86	4.00	5250	0.902	0.842	0.740
21	4.50	3750	0.712	0.725	0.680	87	4.50	5250	0.892	0.839	0.742
22	5.00	3750	0.683	0.682	0.638	88	5.00	5250	0.876	0.832	0.743
23	0.00	4000	0.932	0.921	0.874	89	0.00	5500	0.817	0.848	0.744
24	0.50	4000	0.938	0.934	0.881	90	0.50	5500	0.810	0.810	0.689
25	1.00	4000	0.943	0.943	0.883	91	1.00	5500	0.827	0.818	0.693
26	1.50	4000	0.943	0.948	0.881	92	1.50	5500	0.841	0.821	0.696
27	2.00	4000	0.935	0.947	0.876	93	2.00	5500	0.853	0.821	0.698
28	2.50	4000	0.919	0.941	0.867	94	2.50	5500	0.862	0.820	0.700
29	3.00	4000	0.895	0.931	0.856	95	3.00	5500	0.870	0.819	0.703
30	3.50	4000	0.864	0.914	0.839	96	3.50	5500	0.876	0.818	0.707
31	4.00	4000	0.821	0.877	0.805	97	4.00	5500	0.877	0.817	0.710
32	4.50	4000	0.764	0.801	0.734	98	4.50	5500	0.874	0.814	0.712
33	5.00	4000	0.715	0.726	0.661	99	5.00	5500	0.866	0.809	0.714
34	0.00	4250	0.966	0.914	0.841	100	0.00	5750	0.795	0.845	0.732
35	0.50	4250	0.974	0.928	0.851	101	0.50	5750	0.810	0.855	0.736
36	1.00	4250	0.979	0.936	0.856	102	1.00	5750	0.791	0.801	0.670
37	1.50	4250	0.981	0.941	0.858	103	1.50	5750	0.799	0.801	0.669
38	2.00	4250	0.977	0.943	0.858	104	2.00	5750	0.809	0.798	0.670
39	2.50	4250	0.966	0.941	0.855	105	2.50	5750	0.821	0.797	0.673
40	3.00	4250	0.947	0.936	0.850	106	3.00	5750	0.830	0.794	0.675
41	3.50	4250	0.919	0.926	0.841	107	3.50	5750	0.838	0.793	0.679
42	4.00	4250	0.883	0.910	0.828	108	4.00	5750	0.844	0.791	0.682
43	4.50	4250	0.836	0.877	0.798	109	4.50	5750	0.847	0.789	0.684
44	5.00	4250	0.782	0.812	0.735	110	5.00	5750	0.845	0.785	0.685
45	0.00	4500	0.946	0.893	0.806	111	4.44	5777	0.842	0.785	0.681
46	0.50	4500	0.963	0.907	0.815	112	0.00	6000	0.775	0.848	0.721
47	1.00	4500	0.973	0.916	0.821	113	0.50	6000	0.784	0.850	0.725
48	1.50	4500	0.977	0.921	0.825	114	1.00	6000	0.795	0.852	0.726
49	2.00	4500	0.975	0.923	0.828	115	1.50	6000	0.763	0.784	0.651
50	2.50	4500	0.968	0.923	0.830	116	2.00	6000	0.770	0.780	0.651
51	3.00	4500	0.956	0.919	0.829	117	2.50	6000	0.777	0.775	0.650
52	3.50	4500	0.937	0.914	0.826	118	3.00	6000	0.787	0.771	0.651
53	4.00	4500	0.911	0.905	0.819	119	3.50	6000	0.797	0.768	0.653
54	4.50	4500	0.878	0.893	0.810	120	4.00	6000	0.805	0.765	0.655
55	5.00	4500	0.840	0.869	0.789	121	4.50	6000	0.811	0.762	0.657
56	0.00	4750	0.902	0.864	0.773	122	5.00	6000	0.814	0.759	0.657
57	0.50	4750	0.929	0.882	0.784	123	0.50	6250	0.762	0.851	0.715
58	1.00	4750	0.945	0.891	0.788	124	1.00	6250	0.765	0.844	0.716
59	1.50	4750	0.956	0.897	0.792	125	1.50	6250	0.772	0.839	0.714
60	2.00	4750	0.959	0.899	0.795	126	2.00	6250	0.737	0.765	0.636
61	2.50	4750	0.956	0.899	0.797	127	2.50	6250	0.738	0.757	0.633
62	3.00	4750	0.949	0.897	0.799	128	3.00	6250	0.746	0.751	0.632
63	3.50	4750	0.936	0.893	0.800	129	3.50	6250	0.755	0.745	0.633
64	4.00	4750	0.917	0.887	0.798	130	4.00	6250	0.764	0.742	0.632
65	4.50	4750	0.893	0.879	0.795	131	4.50	6250	0.773	0.738	0.633
66	5.00	4750	0.864	0.869	0.789	132	5.00	6250	0.779	0.734	0.633
						133	0.50	6500	0.739	0.848	0.707
						134	1.00	6500	0.741	0.843	0.707

287	2.50	12500	0.488	0.515	0.450	349	4.50	22000	0.354	0.360	0.318
288	3.00	12500	0.469	0.500	0.434	350	5.00	22000	0.344	0.348	0.311
289	3.50	12500	0.459	0.490	0.426	351	3.00	23000	0.431	0.436	0.392
290	4.00	12500	0.450	0.483	0.424	352	3.50	23000	0.390	0.393	0.348
291	4.50	12500	0.444	0.477	0.423	353	4.00	23000	0.366	0.368	0.326
292	5.00	12500	0.440	0.471	0.424	354	4.50	23000	0.351	0.353	0.313
293	2.50	13000	0.482	0.509	0.444	355	5.00	23000	0.341	0.342	0.305
294	3.00	13000	0.461	0.491	0.426	356	3.00	24000	0.436	0.441	0.398
295	3.50	13000	0.448	0.479	0.416	357	3.50	24000	0.386	0.389	0.345
296	4.00	13000	0.439	0.471	0.412	358	4.00	24000	0.361	0.363	0.321
297	4.50	13000	0.433	0.464	0.411	359	4.50	24000	0.347	0.347	0.308
298	5.00	13000	0.429	0.458	0.412	360	5.00	24000	0.337	0.335	0.301
299	2.00	14000	0.515	0.532	0.479	361	3.00	25000	0.444	0.446	0.407
300	2.50	14000	0.475	0.500	0.437	362	3.50	25000	0.386	0.388	0.345
301	3.00	14000	0.449	0.476	0.413	363	4.00	25000	0.357	0.357	0.316
302	3.50	14000	0.431	0.460	0.399	364	4.50	25000	0.342	0.340	0.303
303	4.00	14000	0.420	0.449	0.393	365	5.00	25000	0.334	0.329	0.296
304	4.50	14000	0.413	0.441	0.390	366	3.00	26000	0.449	0.450	0.414
305	5.00	14000	0.410	0.435	0.391	367	3.50	26000	0.388	0.390	0.347
306	2.50	15000	0.473	0.494	0.434	368	4.00	26000	0.354	0.354	0.314
307	3.00	15000	0.441	0.466	0.404	369	4.50	26000	0.337	0.334	0.298
308	3.50	15000	0.420	0.446	0.387	370	5.00	26000	0.329	0.322	0.291
309	4.00	15000	0.406	0.433	0.378	371	3.50	27000	0.392	0.392	0.351
310	4.50	15000	0.398	0.423	0.374	372	4.00	27000	0.353	0.352	0.313
311	5.00	15000	0.393	0.415	0.373	373	4.50	27000	0.334	0.329	0.294
312	2.50	16000	0.473	0.491	0.434	374	5.00	27000	0.325	0.316	0.286
313	3.00	16000	0.437	0.459	0.399	375	3.50	28000	0.392	0.392	0.353
314	3.50	16000	0.413	0.436	0.378	376	4.00	28000	0.353	0.352	0.313
315	4.00	16000	0.397	0.421	0.366	377	4.50	28000	0.331	0.326	0.292
316	4.50	16000	0.386	0.409	0.360	378	5.00	28000	0.320	0.311	0.281
317	5.00	16000	0.380	0.400	0.358	379	3.50	29000	0.392	0.391	0.354
318	2.50	17000	0.476	0.489	0.436	380	4.00	29000	0.353	0.351	0.313
319	3.00	17000	0.435	0.454	0.395	381	4.50	29000	0.329	0.324	0.289
320	3.50	17000	0.407	0.428	0.371	382	5.00	29000	0.317	0.307	0.277
321	4.00	17000	0.389	0.411	0.358	383	3.50	30000	0.390	0.388	0.352
322	4.50	17000	0.377	0.398	0.35	384	4.00	30000	0.352	0.349	0.311
323	5.00	17000	0.370	0.387	0.346	385	4.50	30000	0.328	0.322	0.288
324	2.50	18000	0.480	0.489	0.440	386	5.00	30000	0.314	0.305	0.274
325	3.00	18000	0.434	0.449	0.394	387	3.50	31000	0.387	0.386	0.351
326	3.50	18000	0.404	0.422	0.366	388	4.00	31000	0.348	0.344	0.308
327	4.00	18000	0.384	0.402	0.351	389	4.50	31000	0.325	0.318	0.284
328	4.50	18000	0.371	0.388	0.342	390	5.00	31000	0.310	0.301	0.271
329	5.00	18000	0.362	0.377	0.337	391	4.00	32000	0.342	0.337	0.303
330	2.50	19000	0.483	0.489	0.443	392	4.50	32000	0.319	0.312	0.280
331	3.00	19000	0.434	0.445	0.392	393	5.00	32000	0.305	0.295	0.266
332	3.50	19000	0.401	0.415	0.363	394	4.00	33000	0.336	0.331	0.298
333	4.00	19000	0.379	0.395	0.344	395	4.50	33000	0.312	0.305	0.274
334	4.50	19000	0.365	0.380	0.334	396	5.00	33000	0.299	0.288	0.261
335	5.00	19000	0.356	0.368	0.329	397	4.00	34000	0.329	0.325	0.292
336	3.00	20000	0.434	0.441	0.392	398	4.50	34000	0.305	0.297	0.267
337	3.50	20000	0.400	0.410	0.359	399	5.00	34000	0.292	0.281	0.254
338	4.00	20000	0.376	0.388	0.340	400	4.00	35000	0.323	0.320	0.287
339	4.50	20000	0.361	0.373	0.328	401	4.50	35000	0.297	0.289	0.260
340	5.00	20000	0.351	0.361	0.322	402	5.00	35000	0.284	0.273	0.247
341	3.00	21000	0.432	0.437	0.390	403	4.00	37500	0.277	0.270	0.242
342	3.50	21000	0.397	0.404	0.356	404	4.50	37500	0.260	0.250	0.226
343	4.00	21000	0.373	0.382	0.335	405	5.00	40000	0.269	0.263	0.233
344	4.50	21000	0.357	0.366	0.323	406	5.00	40000	0.242	0.233	0.209
345	5.00	21000	0.347	0.354	0.316	407	5.00	42500	0.234	0.226	0.201
346	3.00	22000	0.430	0.435	0.389	408	5.00	45000	0.231	0.223	0.197
347	3.50	22000	0.394	0.398	0.352	409	5.00	47500	0.228	0.220	0.194
348	4.00	22000	0.370	0.375	0.331	410	5.00	50000	0.226	0.217	0.192

APPENDIX 6: Table of $u_{\theta}[L]$ and $u_{\theta}[N]$

Table van Hamme

No	log(g) cm/s ²	Teff K	u(L)	u(N)					
					65	4.5	4750	0.201	0.093
					66	5.0	4750	0.201	0.094
1	0.0	3500	0.242	0.117	67	0.0	5000	0.174	0.097
2	0.5	3500	0.240	0.113	68	0.5	5000	0.176	0.093
3	1.0	3500	0.238	0.111	69	1.0	5000	0.179	0.091
4	1.5	3500	0.235	0.108	70	1.5	5000	0.181	0.090
5	2.0	3500	0.233	0.106	71	2.0	5000	0.182	0.091
6	2.5	3500	0.231	0.105	72	2.5	5000	0.186	0.090
7	3.0	3500	0.222	0.104	73	3.0	5000	0.188	0.090
8	3.5	3500	0.184	0.094	74	3.5	5000	0.189	0.089
9	4.0	3500	0.137	0.083	75	4.0	5000	0.191	0.090
10	4.5	3500	0.116	0.077	76	4.5	5000	0.192	0.089
11	5.0	3500	0.106	0.074	77	5.0	5000	0.193	0.089
12	0.0	3750	0.237	0.120	78	0.0	5250	0.161	0.092
13	0.5	3750	0.236	0.118	79	0.5	5250	0.163	0.090
14	1.0	3750	0.235	0.115	80	1.0	5250	0.166	0.088
15	1.5	3750	0.233	0.112	81	1.5	5250	0.168	0.087
16	2.0	3750	0.232	0.111	82	2.0	5250	0.171	0.087
17	2.5	3750	0.231	0.109	83	2.5	5250	0.175	0.085
18	3.0	3750	0.229	0.107	84	3.0	5250	0.177	0.086
19	3.5	3750	0.219	0.104	85	3.5	5250	0.180	0.084
20	4.0	3750	0.184	0.095	86	4.0	5250	0.182	0.085
21	4.5	3750	0.143	0.086	87	4.5	5250	0.183	0.085
22	5.0	3750	0.120	0.079	88	5.0	5250	0.185	0.085
23	0.0	4000	0.228	0.117	89	0.0	5500	0.165	0.082
24	0.5	4000	0.227	0.116	90	0.5	5500	0.149	0.088
25	1.0	4000	0.226	0.114	91	1.0	5500	0.151	0.085
26	1.5	4000	0.226	0.111	92	1.5	5500	0.153	0.085
27	2.0	4000	0.226	0.110	93	2.0	5500	0.158	0.085
28	2.5	4000	0.226	0.109	94	2.5	5500	0.162	0.082
29	3.0	4000	0.226	0.108	95	3.0	5500	0.167	0.082
30	3.5	4000	0.224	0.107	96	3.5	5500	0.170	0.081
31	4.0	4000	0.214	0.104	97	4.0	5500	0.173	0.081
32	4.5	4000	0.183	0.096	98	4.5	5500	0.175	0.081
33	5.0	4000	0.147	0.088	99	5.0	5500	0.176	0.081
34	0.0	4250	0.216	0.111	100	0.0	5750	0.159	0.079
35	0.5	4250	0.216	0.110	101	0.5	5750	0.157	0.077
36	1.0	4250	0.215	0.110	102	1.0	5750	0.140	0.082
37	1.5	4250	0.215	0.107	103	1.5	5750	0.144	0.081
38	2.0	4250	0.216	0.106	104	2.0	5750	0.148	0.080
39	2.5	4250	0.217	0.105	105	2.5	5750	0.152	0.080
40	3.0	4250	0.218	0.104	106	3.0	5750	0.157	0.079
41	3.5	4250	0.218	0.105	107	3.5	5750	0.161	0.078
42	4.0	4250	0.217	0.104	108	4.0	5750	0.165	0.077
43	4.5	4250	0.209	0.102	109	4.5	5750	0.166	0.077
44	5.0	4250	0.182	0.097	110	5.0	5750	0.168	0.078
45	0.0	4500	0.203	0.105	111	0.0	6000	0.154	0.077
46	0.5	4500	0.202	0.103	112	0.5	6000	0.150	0.074
47	1.0	4500	0.203	0.103	113	1.0	6000	0.150	0.072
48	1.5	4500	0.203	0.102	114	1.5	6000	0.134	0.080
49	2.0	4500	0.205	0.101	115	2.0	6000	0.137	0.078
50	2.5	4500	0.207	0.100	116	2.5	6000	0.142	0.077
51	3.0	4500	0.208	0.100	117	3.0	6000	0.147	0.076
52	3.5	4500	0.209	0.099	118	3.5	6000	0.152	0.075
53	4.0	4500	0.210	0.098	119	4.0	6000	0.156	0.075
54	4.5	4500	0.210	0.099	120	4.5	6000	0.158	0.075
55	5.0	4500	0.202	0.098	121	5.0	6000	0.160	0.075
56	0.0	4750	0.189	0.101	122	0.5	6250	0.144	0.071
57	0.5	4750	0.192	0.098	123	1.0	6250	0.143	0.070
58	1.0	4750	0.191	0.095	124	1.5	6250	0.144	0.069
59	1.5	4750	0.193	0.095	125	2.0	6250	0.132	0.076
60	2.0	4750	0.195	0.095	126	2.5	6250	0.134	0.075
61	2.5	4750	0.196	0.095	127	3.0	6250	0.139	0.074
62	3.0	4750	0.198	0.095	128	3.5	6250	0.143	0.073
63	3.5	4750	0.200	0.094	129	4.0	6250	0.147	0.072
64	4.0	4750	0.201	0.094	130	4.5	6250	0.151	0.071

131	5.0	6250	0.153	0.071	207	4.5	8250	0.108	0.054
132	0.5	6500	0.141	0.070	208	5.0	8250	0.110	0.054
133	1.0	6500	0.137	0.067	209	1.0	8500	0.144	0.067
134	1.5	6500	0.137	0.066	210	1.5	8500	0.116	0.057
135	2.0	6500	0.139	0.066	211	2.0	8500	0.107	0.054
136	2.5	6500	0.131	0.071	212	2.5	8500	0.102	0.053
137	3.0	6500	0.133	0.071	213	3.0	8500	0.100	0.051
138	3.5	6500	0.137	0.070	214	3.5	8500	0.100	0.051
139	4.0	6500	0.141	0.069	215	4.0	8500	0.101	0.052
140	4.5	6500	0.144	0.068	216	4.5	8500	0.102	0.052
141	5.0	6500	0.146	0.068	217	5.0	8500	0.105	0.052
142	0.5	6750	0.140	0.069	218	1.5	8750	0.118	0.057
143	1.0	6750	0.132	0.065	219	2.0	8750	0.106	0.052
144	1.5	6750	0.130	0.064	220	2.5	8750	0.100	0.051
145	2.0	6750	0.132	0.063	221	3.0	8750	0.097	0.050
146	2.5	6750	0.134	0.063	222	3.5	8750	0.096	0.050
147	3.0	6750	0.129	0.067	223	4.0	8750	0.096	0.049
148	3.5	6750	0.131	0.068	224	4.5	8750	0.097	0.050
149	4.0	6750	0.134	0.067	225	5.0	8750	0.100	0.050
150	4.5	6750	0.138	0.066	226	1.5	9000	0.121	0.057
151	5.0	6750	0.140	0.066	227	2.0	9000	0.106	0.051
152	0.5	7000	0.140	0.069	228	2.5	9000	0.099	0.049
153	1.0	7000	0.130	0.064	229	3.0	9000	0.095	0.048
154	1.5	7000	0.126	0.062	230	3.5	9000	0.093	0.048
155	2.0	7000	0.126	0.061	231	4.0	9000	0.093	0.048
156	2.5	7000	0.127	0.061	232	4.5	9000	0.093	0.049
157	3.0	7000	0.129	0.061	233	5.0	9000	0.094	0.050
158	3.5	7000	0.128	0.064	234	2.0	9250	0.106	0.051
159	4.0	7000	0.130	0.065	235	2.5	9250	0.098	0.048
160	4.5	7000	0.132	0.065	236	3.0	9250	0.094	0.046
161	5.0	7000	0.135	0.064	237	3.5	9250	0.091	0.046
162	0.5	7250	0.142	0.072	238	4.0	9250	0.090	0.047
163	1.0	7250	0.129	0.063	239	4.5	9250	0.090	0.047
164	1.5	7250	0.123	0.061	240	5.0	9250	0.090	0.048
165	2.0	7250	0.121	0.059	241	2.0	9500	0.106	0.051
166	2.5	7250	0.122	0.059	242	2.5	9500	0.097	0.047
167	3.0	7250	0.123	0.059	243	3.0	9500	0.092	0.045
168	3.5	7250	0.125	0.061	244	3.5	9500	0.090	0.044
169	4.0	7250	0.126	0.063	245	4.0	9500	0.088	0.045
170	4.5	7250	0.127	0.063	246	4.5	9500	0.087	0.045
171	5.0	7250	0.130	0.063	247	5.0	9500	0.087	0.046
172	0.5	7500	0.146	0.073	248	2.0	9750	0.107	0.051
173	1.0	7500	0.128	0.065	249	2.5	9750	0.097	0.047
174	1.5	7500	0.121	0.062	250	3.0	9750	0.091	0.045
175	2.0	7500	0.118	0.058	251	3.5	9750	0.088	0.044
176	2.5	7500	0.117	0.057	252	4.0	9750	0.087	0.043
177	3.0	7500	0.118	0.057	253	4.5	9750	0.086	0.044
178	3.5	7500	0.119	0.059	254	5.0	9750	0.085	0.045
179	4.0	7500	0.121	0.058	255	2.0	10000	0.107	0.052
180	4.5	7500	0.124	0.061	256	2.5	10000	0.096	0.047
181	5.0	7500	0.126	0.061	257	3.0	10000	0.090	0.044
182	1.0	7750	0.128	0.064	258	3.5	10000	0.087	0.043
183	1.5	7750	0.119	0.060	259	4.0	10000	0.085	0.043
184	2.0	7750	0.114	0.059	260	4.5	10000	0.084	0.043
185	2.5	7750	0.113	0.058	261	5.0	10000	0.084	0.044
186	3.0	7750	0.113	0.057	262	2.0	10500	0.105	0.052
187	3.5	7750	0.114	0.057	263	2.5	10500	0.095	0.046
188	4.0	7750	0.116	0.056	264	3.0	10500	0.089	0.043
189	4.5	7750	0.121	0.059	265	3.5	10500	0.085	0.042
190	5.0	7750	0.123	0.059	266	4.0	10500	0.083	0.041
191	1.0	8000	0.130	0.066	267	4.5	10500	0.082	0.041
192	1.5	8000	0.117	0.059	268	5.0	10500	0.081	0.042
193	2.0	8000	0.111	0.057	269	2.5	11000	0.092	0.047
194	2.5	8000	0.109	0.056	270	3.0	11000	0.086	0.043
195	3.0	8000	0.109	0.055	271	3.5	11000	0.083	0.041
196	3.5	8000	0.109	0.055	272	4.0	11000	0.081	0.040
197	4.0	8000	0.111	0.055	273	4.5	11000	0.080	0.040
198	4.5	8000	0.113	0.055	274	5.0	11000	0.079	0.040
199	5.0	8000	0.120	0.056	275	2.5	11500	0.090	0.046
200	1.0	8250	0.134	0.065	276	3.0	11500	0.084	0.043
201	1.5	8250	0.116	0.059	277	3.5	11500	0.080	0.041
202	2.0	8250	0.109	0.055	278	4.0	11500	0.079	0.039
203	2.5	8250	0.105	0.054	279	4.5	11500	0.078	0.039
204	3.0	8250	0.104	0.053	280	5.0	11500	0.077	0.040
205	3.5	8250	0.105	0.053	281	2.5	12000	0.087	0.047
206	4.0	8250	0.106	0.054	282	3.0	12000	0.081	0.043

283	3.5	12000	0.078	0.041	359	4.5	24000	0.063	0.042
284	4.0	12000	0.076	0.039	360	5.0	24000	0.061	0.041
285	4.5	12000	0.075	0.038	361	3.0	25000	0.091	0.053
286	5.0	12000	0.075	0.038	362	3.5	25000	0.075	0.047
287	2.5	12500	0.085	0.046	363	4.0	25000	0.068	0.044
288	3.0	12500	0.078	0.043	364	4.5	25000	0.064	0.042
289	3.5	12500	0.075	0.040	365	5.0	25000	0.062	0.041
290	4.0	12500	0.074	0.039	366	3.0	26000	0.094	0.054
291	4.5	12500	0.073	0.038	367	3.5	26000	0.075	0.047
292	5.0	12500	0.072	0.038	368	4.0	26000	0.069	0.044
293	2.5	13000	0.084	0.046	369	4.5	26000	0.065	0.042
294	3.0	13000	0.076	0.042	370	5.0	26000	0.064	0.041
295	3.5	13000	0.073	0.040	371	3.5	27000	0.076	0.046
296	4.0	13000	0.071	0.039	372	4.0	27000	0.069	0.043
297	4.5	13000	0.070	0.038	373	4.5	27000	0.066	0.041
298	5.0	13000	0.070	0.037	374	5.0	27000	0.064	0.040
299	2.0	14000	0.103	0.054	375	3.5	28000	0.077	0.046
300	2.5	14000	0.083	0.046	376	4.0	28000	0.069	0.043
301	3.0	14000	0.074	0.042	377	4.5	28000	0.065	0.041
302	3.5	14000	0.070	0.040	378	5.0	28000	0.064	0.039
303	4.0	14000	0.068	0.038	379	3.5	29000	0.077	0.046
304	4.5	14000	0.067	0.037	380	4.0	29000	0.069	0.042
305	5.0	14000	0.067	0.037	381	4.5	29000	0.065	0.041
306	2.5	15000	0.083	0.047	382	5.0	29000	0.063	0.039
307	3.0	15000	0.072	0.042	383	3.5	30000	0.077	0.046
308	3.5	15000	0.067	0.040	384	4.0	30000	0.068	0.042
309	4.0	15000	0.065	0.038	385	4.5	30000	0.064	0.040
310	4.5	15000	0.064	0.037	386	5.0	30000	0.062	0.039
311	5.0	15000	0.064	0.037	387	3.5	31000	0.077	0.047
312	2.5	16000	0.084	0.047	388	4.0	31000	0.067	0.041
313	3.0	16000	0.072	0.042	389	4.5	31000	0.063	0.039
314	3.5	16000	0.066	0.039	390	5.0	31000	0.061	0.038
315	4.0	16000	0.063	0.038	391	4.0	32000	0.066	0.042
316	4.5	16000	0.062	0.038	392	4.5	32000	0.061	0.039
317	5.0	16000	0.061	0.037	393	5.0	32000	0.059	0.037
318	2.5	17000	0.086	0.049	394	4.0	33000	0.065	0.043
319	3.0	17000	0.072	0.042	395	4.5	33000	0.060	0.039
320	3.5	17000	0.065	0.039	396	5.0	33000	0.057	0.037
321	4.0	17000	0.061	0.038	397	4.0	34000	0.065	0.044
322	4.5	17000	0.060	0.037	398	4.5	34000	0.059	0.039
323	5.0	17000	0.060	0.037	399	5.0	34000	0.056	0.037
324	2.5	18000	0.090	0.051	400	4.0	35000	0.065	0.044
325	3.0	18000	0.072	0.044	401	4.5	35000	0.058	0.040
326	3.5	18000	0.064	0.040	402	5.0	35000	0.054	0.037
327	4.0	18000	0.060	0.038	403	4.5	37500	0.056	0.042
328	4.5	18000	0.059	0.037	404	5.0	37500	0.052	0.040
329	5.0	18000	0.058	0.037	405	4.5	40000	0.054	0.042
330	2.5	19000	0.096	0.055	406	5.0	40000	0.050	0.040
331	3.0	19000	0.074	0.045	407	5.0	42500	0.049	0.041
332	3.5	19000	0.065	0.041	408	5.0	45000	0.049	0.040
333	4.0	19000	0.060	0.038	409	5.0	47500	0.049	0.041
334	4.5	19000	0.058	0.037	410	5.0	50000	0.049	0.041
335	5.0	19000	0.057	0.037					
336	3.0	20000	0.077	0.047					
337	3.5	20000	0.066	0.042					
338	4.0	20000	0.060	0.039					
339	4.5	20000	0.058	0.038					
340	5.0	20000	0.057	0.037					
341	3.0	21000	0.080	0.050					
342	3.5	21000	0.067	0.044					
343	4.0	21000	0.061	0.041					
344	4.5	21000	0.058	0.039					
345	5.0	21000	0.057	0.038					
346	3.0	22000	0.084	0.052					
347	3.5	22000	0.070	0.046					
348	4.0	22000	0.063	0.042					
349	4.5	22000	0.059	0.041					
350	5.0	22000	0.058	0.040					
351	3.0	23000	0.086	0.053					
352	3.5	23000	0.072	0.047					
353	4.0	23000	0.065	0.043					
354	4.5	23000	0.061	0.041					
355	5.0	23000	0.059	0.040					
356	3.0	24000	0.088	0.053					
357	3.5	24000	0.074	0.047					
358	4.0	24000	0.067	0.044					